



## DAMAGE ASSESSMENT OF EXPRESSWAY NETWORKS IN JAPAN BASED ON SEISMIC MONITORING

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### SUMMARY

Fragility curves for expressway structures in Japan were proposed based on actual damage data from the 1995 Hyogoken-Nanbu (Kobe) Earthquake. First, spatial distributions of strong motion indices, e.g., the peak ground acceleration, the peak ground velocity, the JMA seismic intensity, were estimated using Kriging technique, in which attenuation relations of these indices are considered as trend components. The actual damage data for expressway structures in Japan due to the 1995 Hyogoken-Nanbu Earthquake were compared with these estimated ground motion indices and then fragility curves were constructed assuming log-normal distributions. Together with a seismic network for the expressway networks, the proposed fragility curves may be used in seismic damage assessment of expressway structures in Japan.

### INTRODUCTION

Japan Highway Public Corporation (JH) owns expressway networks with a total length of 6,456 km (as of April, 1999). In order to gather earthquake information at an early stage (Yamazaki et al., 1998) and to establish an efficient traffic control just after an earthquake, JH had deployed 123 accelerometers along its expressways (1 instrument per 40 km) before the Hyogoken-Nanbu (Kobe) Earthquake on January 17, 1995. JH further deployed 202 new seismometers along its expressways (1 instrument per 20 km together with existing ones) after the Hyogoken-Nanbu Earthquake (Fig. 1). The new instruments can measure the spectrum intensity (SI) and the instrumental JMA (Japan Meteorological Agency) intensity (Shabestari and Yamazaki, 1998) as well as the peak ground acceleration (PGA).

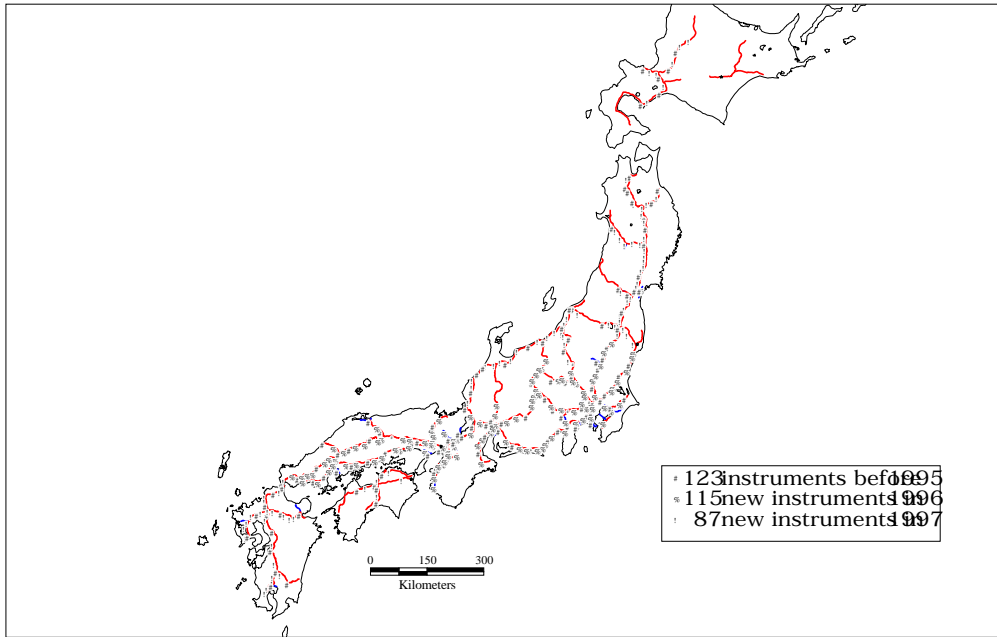
Using earthquake information from these instruments, JH closes expressways if the PGA equal or larger than 80  $\text{cm/s}^2$  is recorded or reduces the maximum speed limit if the PGA equal or larger than 50  $\text{cm/s}^2$  is recorded. These traffic regulations continue until safety inspections for roadways are completed. But these current regulation criteria need to be examined considering the increase of number of instruments, the higher sensitivity of new instruments and the recent experiences for damaging and non-damaging earthquakes.

Hence, it may be important to clarify the relationship between the earthquake damage to expressway structures and the strong ground motion indices. In this study, the damage data of the JH's expressway structures in the Hyogoken-Nanbu Earthquake were collected and the ground motion indices along the expressways were estimated based on observed records using Kriging technique. Comparing these results, fragility curves for the expressway structures (bridges and elevated structures) in Japan were constructed. The proposed fragility curves may be used for damage estimation of expressway structures in Japan. Note that a study on bridge fragility in the United States is found in Kiremidjian and Bosöz (1997) and a study on damage estimation of national highway bridges in Japan was conducted by Sugita and Hamada (1997).

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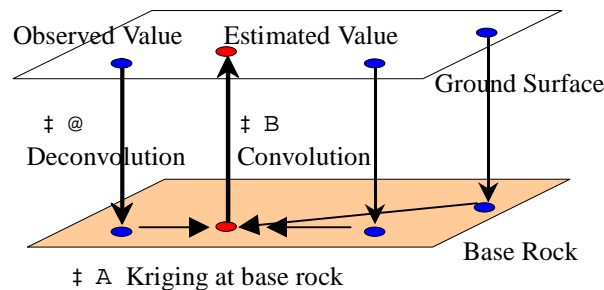
**Figure 1: Location of accelerometers for expressway networks in Japan**

### **SPATIAL DISTRIBUTION OF EARTHQUAKE GROUND MOTION**

The method to estimate spatial distribution of earthquake ground motion suitable for expressway networks is proposed. Earthquake information currently obtained just after an earthquake is ground motion indices (PGA, SI and JMA intensity) recorded by the instruments connected to traffic control centers by private lines. Acceleration time histories are collected later manually. The magnitude and hypocenter of an event are informed by the Japan Meteorological Agency (JMA) within a few minutes after the occurrence of an earthquake.

Kriging technique (Cressie, 1993; Deutsch and Journel, 1992), a method of stochastic interpolation, is employed to estimate spatial distribution of ground motion indices from recorded values. In Kriging technique, observed values are realized at the observation points. Between the observation points, stochastic interpolation consisting of the trend (mean) and random components gives an estimation of the spatial distribution.

Since the earthquake motion at a ground surface is affected by amplification characteristics of subsurface layers, the interpolation should be carried out at the (outcrop) base as shown in Fig. 2. The amplification ratio (Yamazaki et. al, 1999) estimated from attenuation relationships and the digital national land information of Japan is used to convert the recorded values at the ground surface to those at the base. After the spatial interpolation by Kriging, the amplification ratio is again introduced and the spatial distribution of the ground motion indices at the ground surface is obtained. Note that in this procedure, the amplification ratio is treated to be deterministic although it contains a large amount of randomness.



**Figure 2: Schematic figure for interpolation of strong motion indices on ground surface and on base rock**

## ESTIMATION OF STRONG MOTION DISTRIBUTION IN THE 1995 HYOGOKEN-NANBU EARTHQUAKE BY KRIGING

### Strong Motion Data

In the 1995 Hyogoken-Nanbu Earthquake, a large number of strong motion records were obtained (Molas and Yamazaki, 1995b). In this study, free field records at 165 sites were used to estimate the spatial distribution of ground motion indices. Among these records, the authors obtained acceleration time histories at 99 sites. The peak ground velocity (PGV) and JMA intensity were calculated for these sites. For the remaining 66 sites, only PGA values were known. Amplification ratios of these indices at the recording sites were estimated from the topography and subsurface soil classification of the digital national land information. Using these amplification ratios, the recorded values at the ground surface were converted to those at the base rock ( $V_s \geq 300\text{-}400$  m/s).

### Attenuation Relations at the Base

Using the converted values at the base level, the simple Kriging method (Deutsch and Journel, 1992) was employed to estimate the spatial distribution of the strong motion indices. In this study, attenuation relations for strong motion indices (Molas and Yamazaki, 1995a; Shabestari and Yamazaki, 1998) were used as the trend component of Kriging. Since the attenuation relations contain the inter-event variability (deviation associated with different earthquakes), it may be preferable to construct an attenuation equation for each event if many observed values exist. For the Hyogoken-Nanbu Earthquake, the following forms including the near-source saturation effect were considered for the strong motion indices:

$$\text{for PGA and PGV: } \log_{10} x = c_1 - \log_{10} (r + c_2) + c_3 r \quad (1)$$

$$\text{for JMA Intensity: } I = c_1 - 1.89 \log_{10} (r + c_2) + c_3 r \quad (2)$$

where  $c_1$ ,  $c_2$ , and  $c_3$  are coefficients to be obtained by regression analyses and  $r$  is the shortest distance (km) to the fault rupture. For the Hyogoken-Nanbu Earthquake, the fault was modeled as a vertical plane stretching in between points (134.92°E, 34.53°N) and (135.32°E, 34.76°N) with the depth of the upper edge 4.5 km (Kamae and Irikura, 1995).

Using the (converted) observed values at 149 sites whose soil classification is estimated, the attenuation relations for the Hyogoken-Nanbu Earthquake at the base were obtained as

$$\text{for PGA: } \log_{10} PGA = 3.808 - \log_{10} (r + 6.3) - 0.00128 r \quad (3)$$

$$\text{for PGV: } \log_{10} PGV = 2.510 - \log_{10} (r + 0.1) \quad (4)$$

$$\text{for JMA Intensity: } I = 7.563 - 1.89 \log_{10} (r + 1.0) - 0.00118 r \quad (5)$$

In equation (4),  $c_3$  was set to be zero since it was obtained as a negative value, which is physically inadmissible.

The obtained relation for PGV is plotted in Fig. 3 together with data points and the attenuation relation proposed by Molas and Yamazaki (1995a). The current relation looks similar as the existing one. For PGA and intensity, near-source saturation effects were clearly observed in the attenuation relationship for the Hyogoken-Nanbu Earthquake.

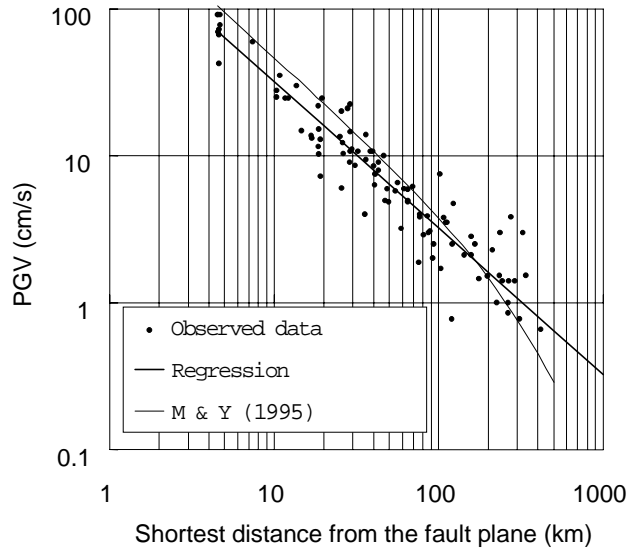
### Method of Kriging

In the Kriging technique, a spatial auto-correlation function should be assigned. An exponential function was employed in this study. The correlation distance, which controls the influence of observed data, was assumed as 5.0 km. Note that if the correlation distance is large, the estimated distribution connects the observed points irrespective of the trend component while if the correlation distance is small, the estimated distribution approaches the trend rapidly. A further research is necessary to determine the spatial auto-correlation function for strong motion indices.

In this study, Kriging technique is employed for the residuals (the converted observed values at the base minus the trend component):

$$\text{for PGA and PGV } X_{zi} = \log_{10} x_{bi} - \log_{10} x_{mi} \quad (6)$$

$$\text{for Intensity } X_{li} = I_{bi} - I_{mi} \quad (7)$$

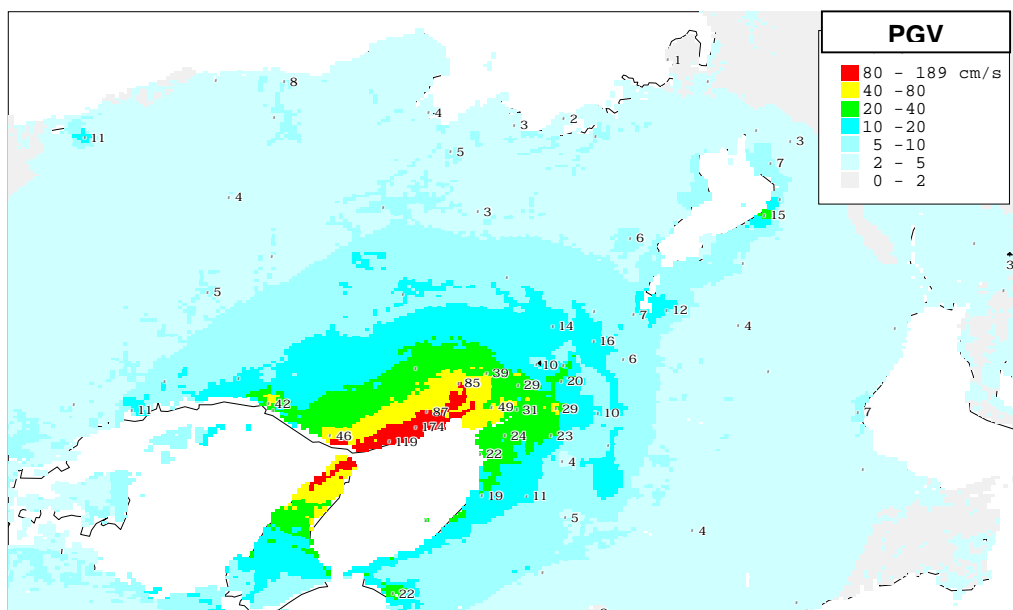


**Figure 3: Attenuation relationship of peak ground velocity (converted to base-rock) in the 1995 Hyogoken-Nanbu Earthquake**

where suffix  $b$  represents “base” and  $m$  represents “mean”. Simple Kriging is carried out assuming the residual distributions as a zero-mean Gaussian stochastic field. Adding the trend component to the obtained random component, the strong motion indices at the base are estimated. Multiplying the amplification factors to the obtained values at the base, the spatial distribution at the ground surface is finally obtained.

#### Spatial Distribution of Ground Motion in the Hyogoken-Nanbu Earthquake

The spatial distributions of PGA, PGV and JMA intensity in the Hyogoken-Nanbu Earthquake were estimated for the area affected by the earthquake. At all the 41,266 grid points corresponding to the 1 km x 1 km pixels of the digital national land information, the ground motion indices were obtained by the method described above. Figure 4 shows the estimated distribution of PGV in the Hyogoken-Nanbu Earthquake together with the observed PGV. The estimated distribution looks quite natural as well as fitting the observed values. The introduction of the attenuation relation to the trend component made this possible.



**Figure 4: Estimated distribution of PGV on ground surface in the Hyogoken-Nanbu Earthquake by Kriging**

## FRAGILITY CURVES FOR EXPRESSWAY BRIDGES

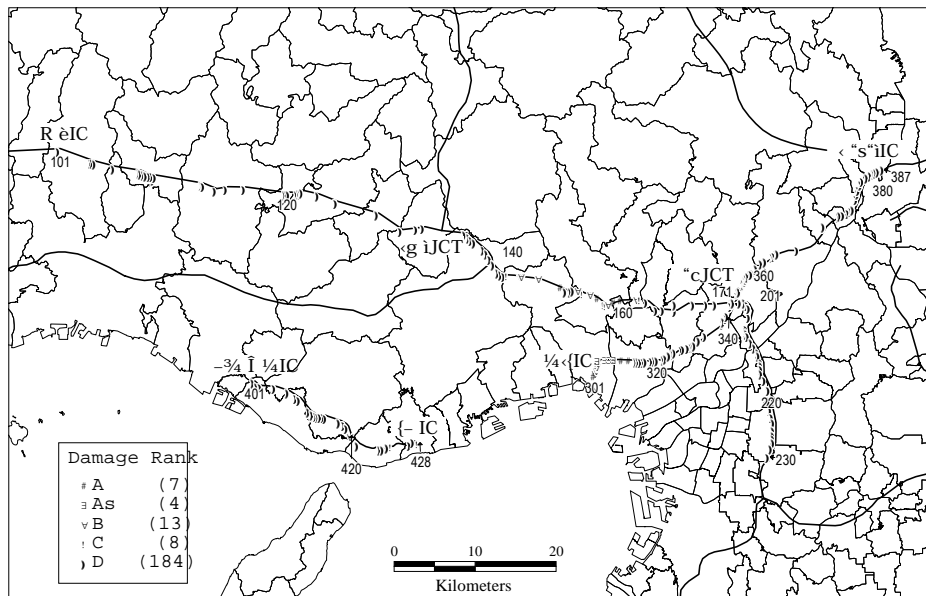
In the Hyogoken-Nanbu Earthquake, tremendous damage occurred to expressway structures and facilities, e.g., bridges and elevated structures, embankments, toll gates. In this study, JH's 216 bridge structures on 4 routes were investigated. In doing this, bridges without damage in the same routes were also considered since they provide useful information. Table 1 summarizes damage ranks of the JH's bridge structures and the locations of the bridges are plotted in Fig. 5. It is seen in the figure that the highest damage rank (As) bridges are concentrated along the Meishin and Chugoku Expressways.

Figure 6 plots the relation between the damage ranks of the bridges along the Chugoku Expressway and the estimated PGV values at the bridge locations obtained by Fig. 5. Significant damage is seen to occur at the locations of large PGV values. A similar comparison was conducted for other routes and the relation between the damage rank and estimated PGV is plotted in Fig. 7 for all the 216 bridges. It is also observed for other strong motion indices (PGA and I) that the damage rank becomes higher as the motion becomes larger.

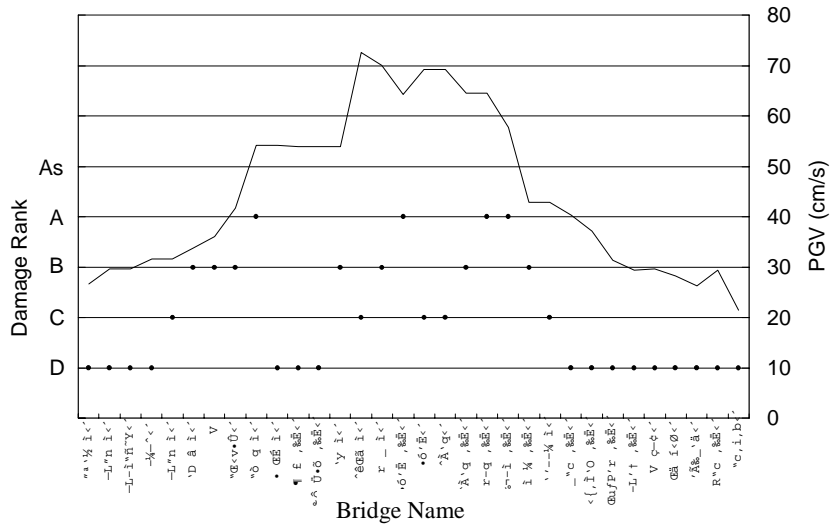
Based on these data, fragility curves for bridge structures are constructed assuming log-normal distributions (normal distribution for the intensity) for the cumulative probability  $P_R$  of occurrence of the damage equal or higher than rank  $R$  as follows:

**Table 1: Damage of JH's expressway bridge structures in the 1995 Hyogoken-Nanbu Earthquake**

Route	Section	Damage Rank of Bridges					Total
		As	A	B	C	D	
Chugoku Expressway	Suita JCT- Yamazaki	4	0	7	5	55	71
Kinki Expressway	Suita JCT- Yao	0	0	0	0	30	30
Meishin Expressway	Nishinomiya - Kyoto S.	3	4	5	1	74	87
Daini Shinmei Road	Suma - Akashi West	0	0	1	2	25	28
Total		7	4	13	8	184	216



**Figure 5: Location and damage rank of JH's expressway bridges in the 1995 Hyogoken-Nanbu Earthquake**

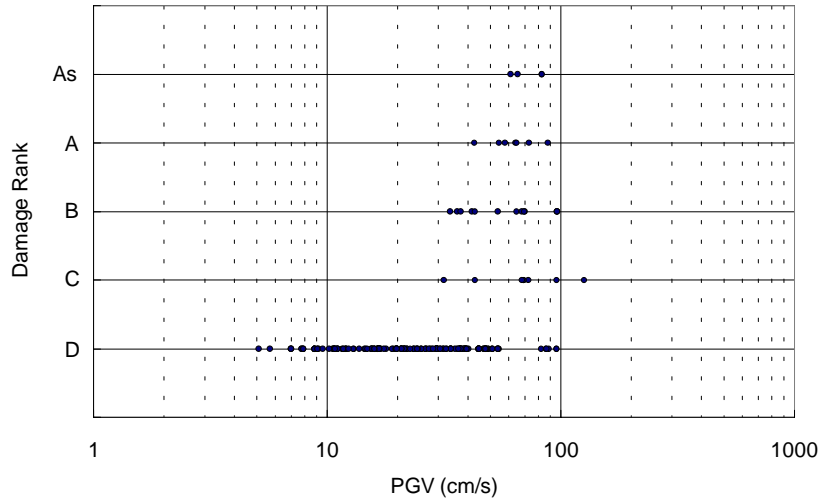


**Figure 6: Relationship between damage rank and estimated PGV for 32 bridges on Chugoku Expressway**

for PGA and PGV  $P_R(x) = \Phi((\ln x - \lambda) / \zeta)$  (10)

for Intensity  $P_R(I) = \Phi((I - \lambda) / \zeta)$  (11)

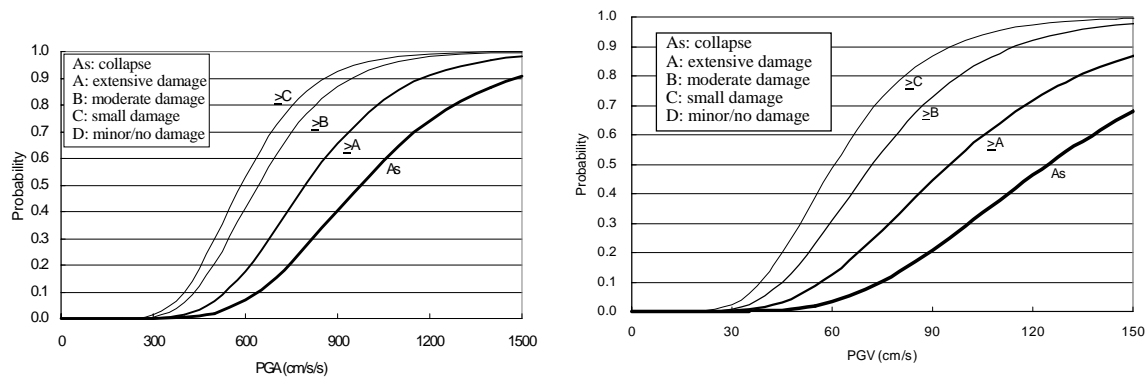
where  $\Phi$  is the standard normal distribution and  $\lambda$  and  $\zeta$  are the mean and standard deviation of  $\ln PGA$ ,  $\ln PGV$  and  $I$ . The two parameters of the distributions are determined by the least square method on the log-normal probability paper and the results are listed in Table 2.



**Figure 7: Relation between damage rank and estimated PGV for JH's 216 bridges in the Hyogoken-Nanbu Earthquake**

**Table 2: Coefficients of fragility curves for expressway bridge structures in Japan**

Damage Rank	PGA (cm/s <sup>2</sup> )		PGV (cm/s)		JMA Intensity	
	$\lambda$	$\zeta$	$\lambda$	$\zeta$	$\lambda$	$\zeta$
$\geq C$	6.36	0.298	4.10	0.352	6.01	0.272
$\geq B$	6.47	0.301	4.28	0.364	6.15	0.292
$\geq A$	6.68	0.305	4.55	0.404	6.36	0.333
As	6.89	0.326	4.82	0.400	6.59	0.352



**Figure 8: Fragility curves of bridge structures for PGA and PGV derived from the damage data due to the Hyogoken-Nanbu Earthquake**

Figure 8 shows the empirical fragility curves of expressway bridge structures in Japan with respect to PGA and PGV. In spite of rather sparse data in Fig. 7, the obtained fragility curves look reasonable. However, it is obvious that the fragility curves are dependent on the seismic code used (Sugita and Hamada, 1997) and the structural type of bridges (Kiremidjian and Bosöz, 1997). Retrofitted bridges may have larger strength than before. Considering these facts, we are currently working on the development of bridge fragility curves considering the structural parameters and strong motion parameters based on numerical simulation (Karim and Yamazaki, 1999). Since the effect of seismic motion to automobile drivers is also considered to be important to establish expressway traffic control criteria, virtual experiments using driving simulators are also in progress (Yamanouchi and Yamazaki, 1999).

## CONCLUSIONS

As a first step for the proposal of appropriate expressway traffic control immediately after earthquakes, the relationship between the strong motion indices and the damage of expressway structures from recent earthquakes in Japan was investigated. First, the spatial distributions of strong motion indices, e.g., the peak ground acceleration, the peak ground velocity, the JMA intensity, were estimated for the 1995 Hyogoken-Nanbu Earthquake using the digital national land information and Kriging technique. In this approach the recorded data are satisfied at the recording sites and the attenuation relations of the strong motion indices are considered as a trend component. The actual damage data for expressway networks in the Hyogoken-Nanbu Earthquake were compared with the estimated ground motion indices and then fragility curves were constructed assuming log-normal distributions. Although the proposed fragility curves are still tentative, they may be used in damage estimation of expressway structures in Japan due to earthquakes. Combining with a seismometer network, the proposed methodology can be easily introduced to a real-time damage assessment of expressway networks.

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