

CE03.98N

Soil Dynamics and Earthquake Engineering

#5 Seismic Hazard and Seismic Risk

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Course Outline (1)

- | | |
|--|--------------------|
| 1. Introduction
1.1 Earthquakes
1.2 Consequences of Earthquakes | Jan. 8 |
| 2. Engineering Seismology
2.1 Mechanism of Earthquakes
2.2 Seismic Waves
2.3 Earthquake Magnitude and Seismic Intensity
2.4 Seismometers and Seismic Observation
2.5 Tsunamis | Jan. 15 |
| 3. Seismic Ground Motion
3.1 Fourier Spectrum
3.2 Characteristics of Seismic Ground Motion
3.3 Response Spectrum
3.4 Attenuation Relations and Effects of Soil Conditions
3.5 Microtremor Observation | Jan. 22
Jan. 29 |

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Course Outline (2)

4. Seismic Hazard and Seismic Risk

- 4.1 Seismic Hazard Analysis
- 4.2 Damage Assessment

Feb. 5

By Prof. F. Yamazaki

5. Dynamic Soil Properties

- 5.1 Measurement of Dynamic Soil Properties
- 5.2 Stress-Strain Behaviors

By Prof. P.K. Basudhar

6. Wave Propagation and Ground Response Analysis

- 6.1 Wave Propagation
- 6.2 One-Dimensional Ground Response Analysis

7. Liquefaction and Slope Stability

- 7.1 Liquefaction
- 7.2 Slope Stability

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4.1 Seismic Hazard Analysis

➤ Deterministic Seismic Hazard Analysis

Ground motion hazard evaluation based on a particular scenario earthquake

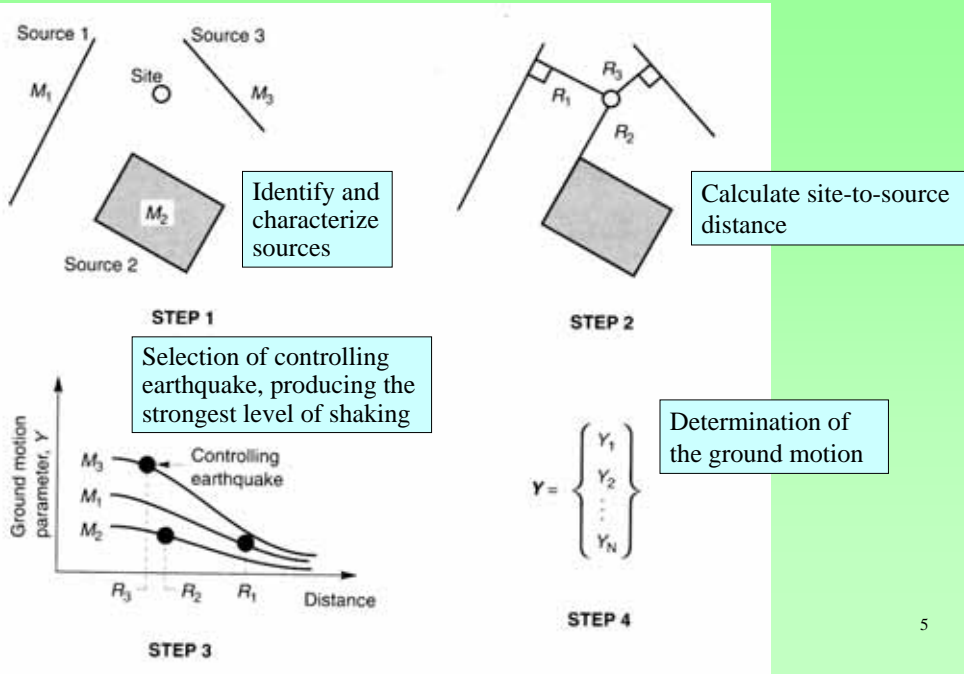
➤ Probabilistic Seismic Hazard Analysis

Considering uncertainties in the size, location, and rate of recurrence of earthquakes.

Developed by Cornell (1968).

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Deterministic Seismic Hazard Analysis

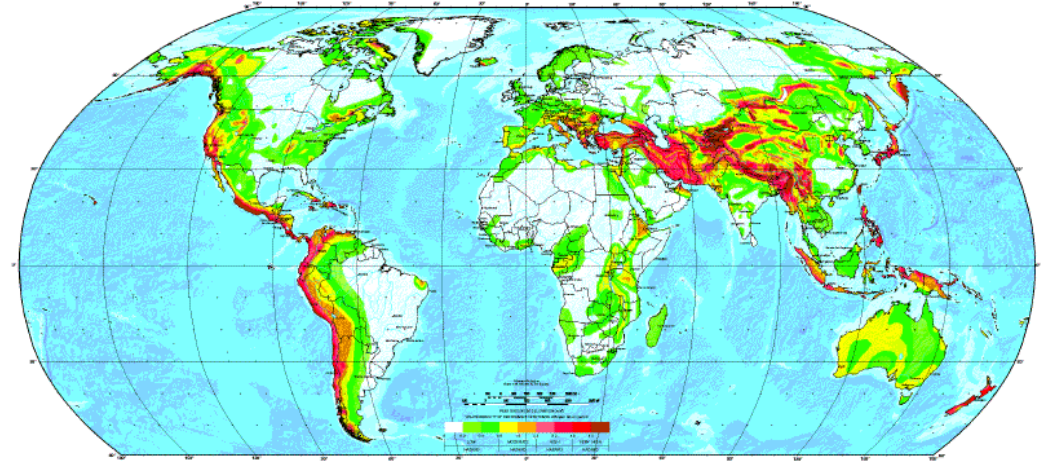


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Earthquake Hazard Map

GLOBAL SEISMIC HAZARD MAP

GLOBAL SEISMIC HAZARD ASSESSMENT PROGRAM



<http://seismo.ethz.ch/gshap/>

Probabilistic Seismic Hazard Analysis

1. Determine potential earthquake sources around a site by points, lines and planes.-(A)
2. Assuming a *Poisson process*, the annual probability P that the intensity parameter Y exceed a value y is

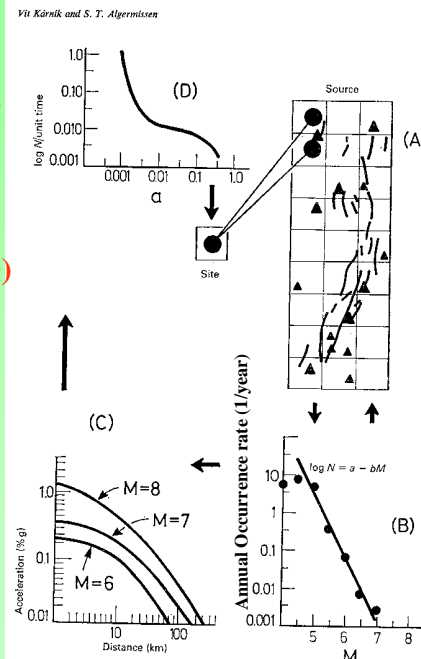
$$P(y) = 1 - \exp \left\{ - \sum_{i=1}^n v_i q_i(y) \right\} \quad \text{-(D)}$$

where n : number of source areas

v_i : earthquake occurrence rate in source i - (B)

q_i : the probability that $Y > y$ when an earthquake occurs in source i
 -- based on an attenuation relation (C) and probability distributions of M and r

3. Hazard curve for a site → Hazard map



Probabilistic Seismic Hazard Analysis

Annual Exceedance Probability

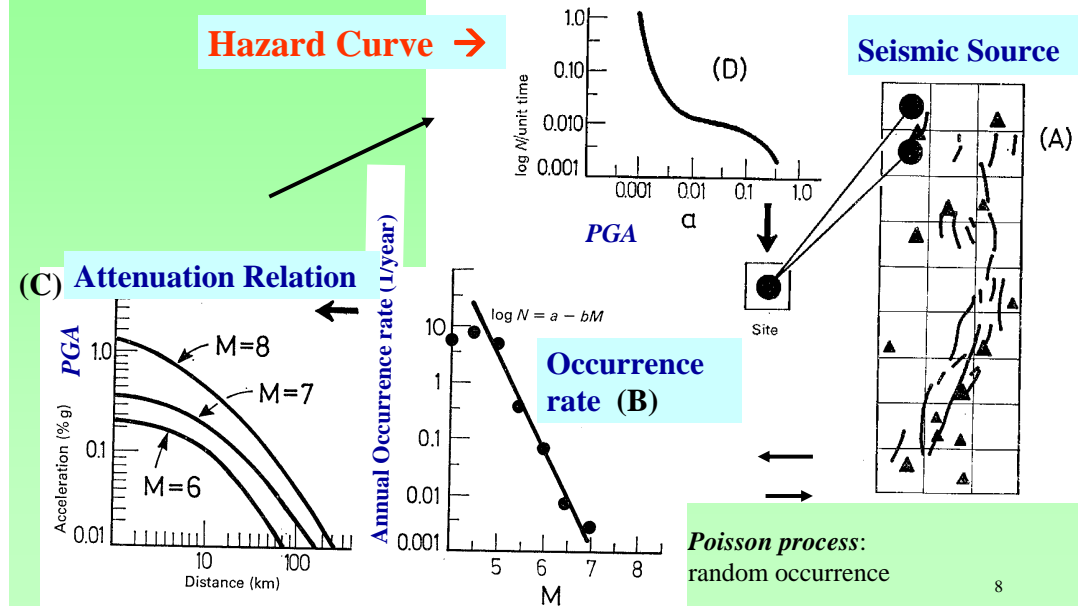
Hazard Curve →

Seismic Source

(C) Attenuation Relation

Annual Occurrence rate (1/year)

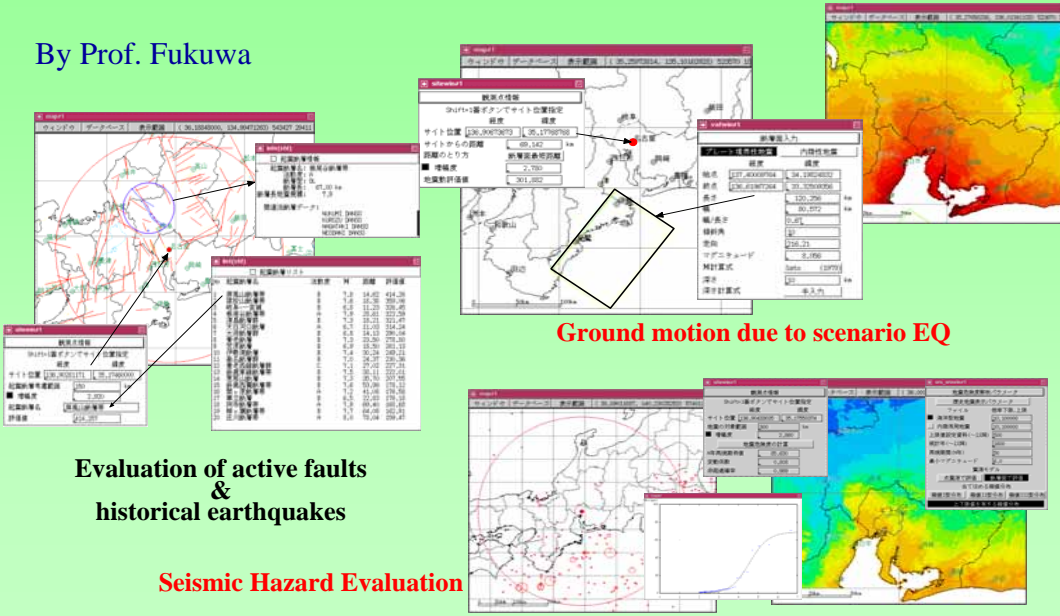
Poisson process: random occurrence



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Database for Seismic Hazard Assessment

By Prof. Fukuwa



Ground motion due to scenario EQ

Evaluation of active faults & historical earthquakes

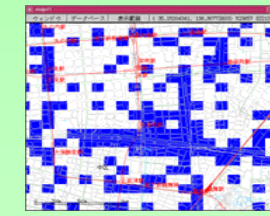
Seismic Hazard Evaluation

Geological Data for Hazard Assessment

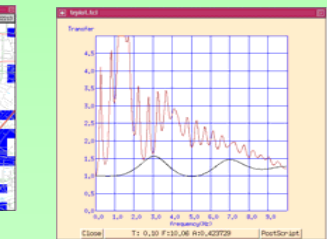
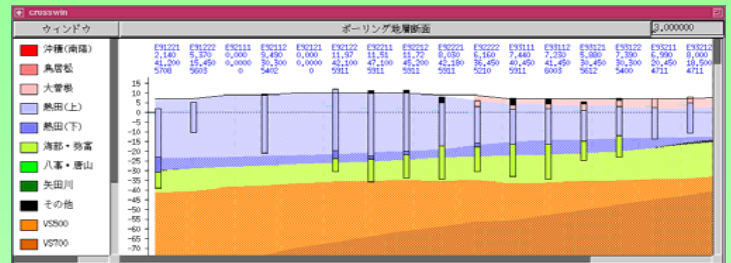
By Prof. Fukuwa

Geologic section

Boring points



Plot with digital map



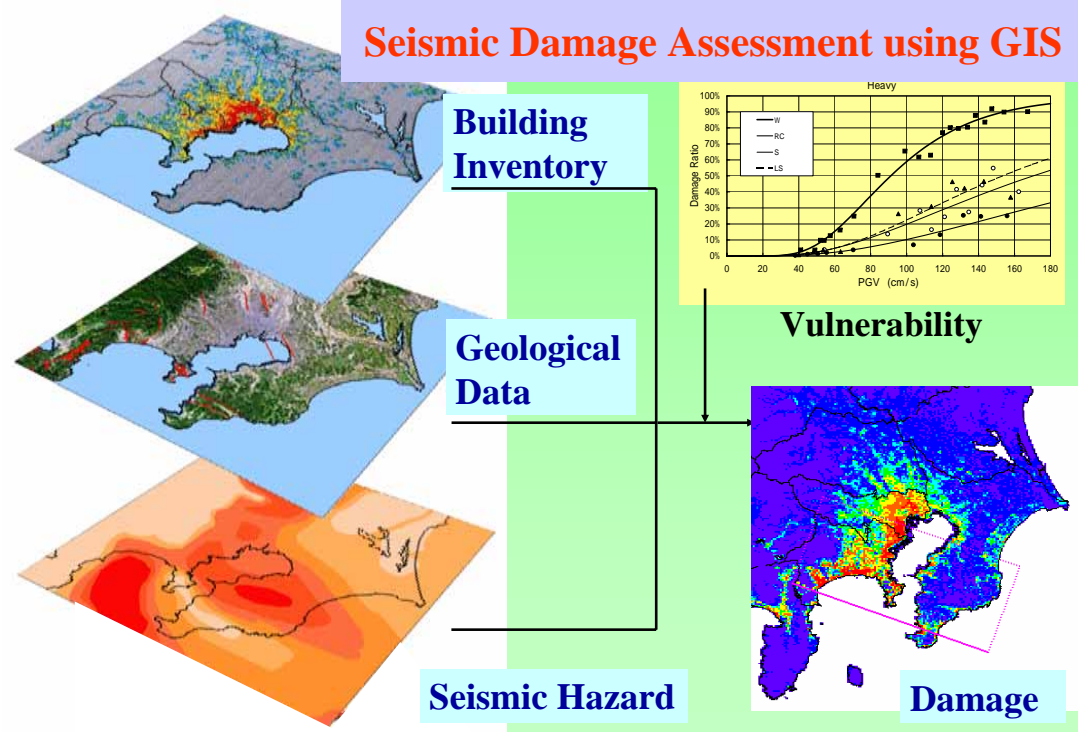
Soil amplification



Boring log

4.2 Damage Assessment

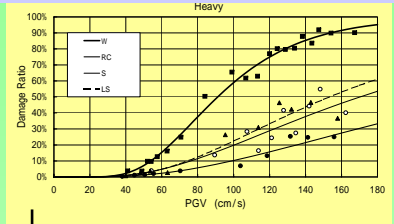
Seismic Damage Assessment using GIS



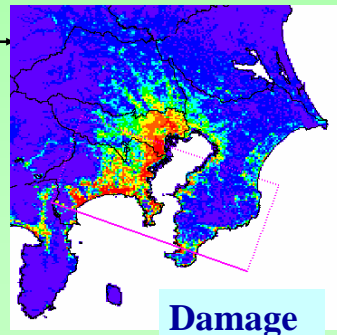
Building Inventory

Geological Data

Seismic Hazard



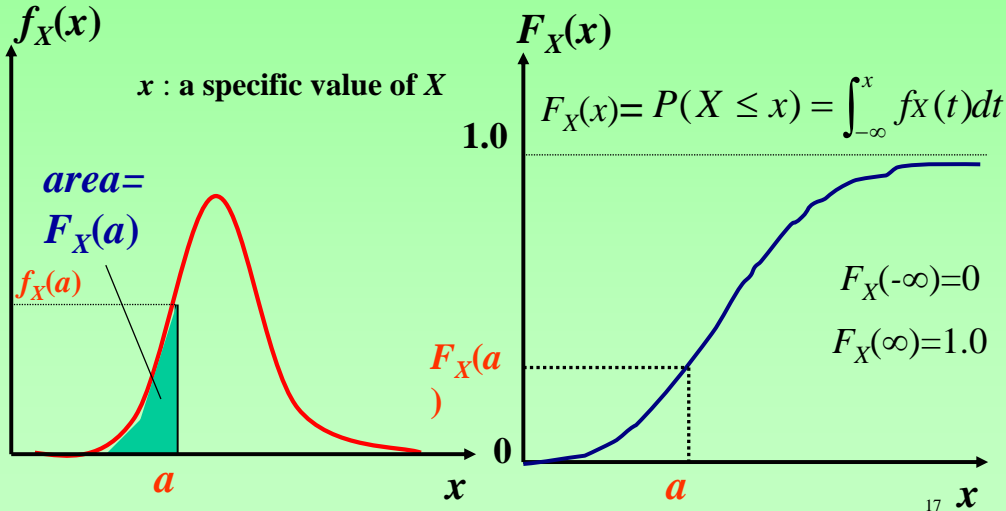
Vulnerability



Damage

Probability distribution of a continuous random variable X

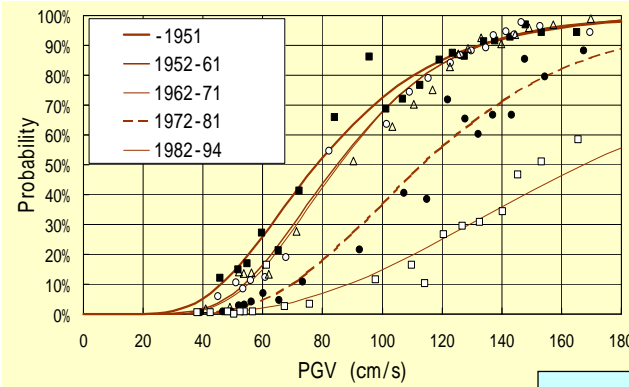
Probability Density Function Cumulative Distribution Function



Fragility Curve = Vulnerability Function

The cumulative distribution function of strength as a function of strong motion indices = **Fragility Curve**

Log-normal distribution:
 $\ln x$ is normal dist.

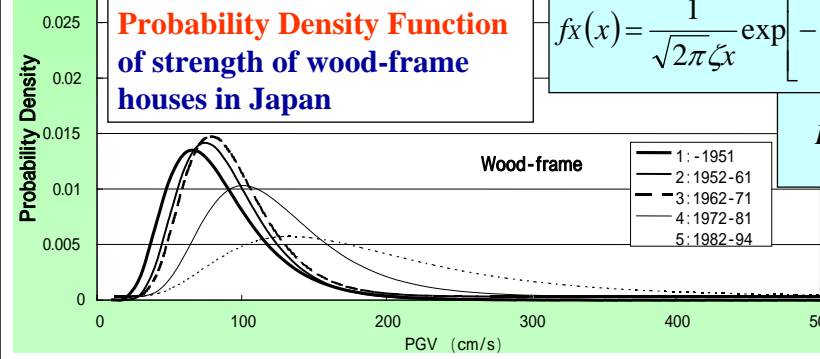


Probability Density Function of strength of wood-frame houses in Japan

$$f_X(x) = \frac{1}{\sqrt{2\pi}\zeta x} \exp\left[-\frac{1}{2}\left(\frac{\ln x - \lambda}{\zeta}\right)^2\right]$$

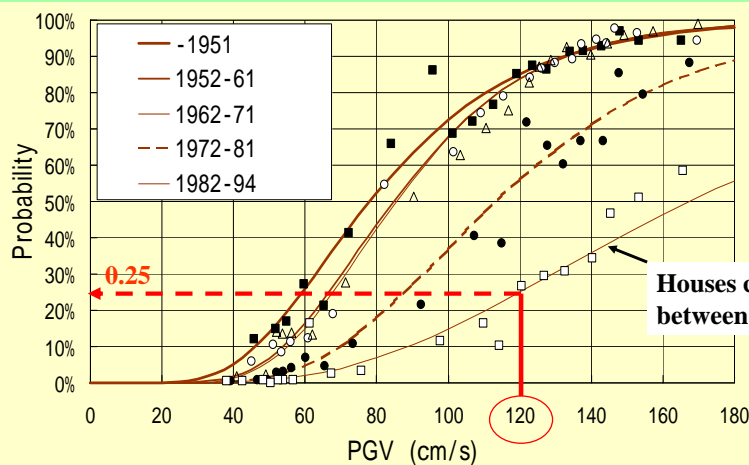
$$F_X(x) = \Phi\left(\frac{\ln x - \lambda}{\zeta}\right)$$

: the standard normal distribution $N(0, 1)$
 λ : mean of $\ln x$
 ζ : standard deviation of $\ln x$



Damage probability of buildings when seismic motion (PGV) is given *deterministically* (a normal case of damage assessment)

If seismic motion is given as $PGV=120\text{cm/s}$, the damage probability of wood-frame houses (1982-94) becomes 25%.



$$F_X(120) = \int_0^{120} f_X(t) dt$$

$$= \Phi\left(\frac{\ln 120 - \lambda}{\zeta}\right)$$

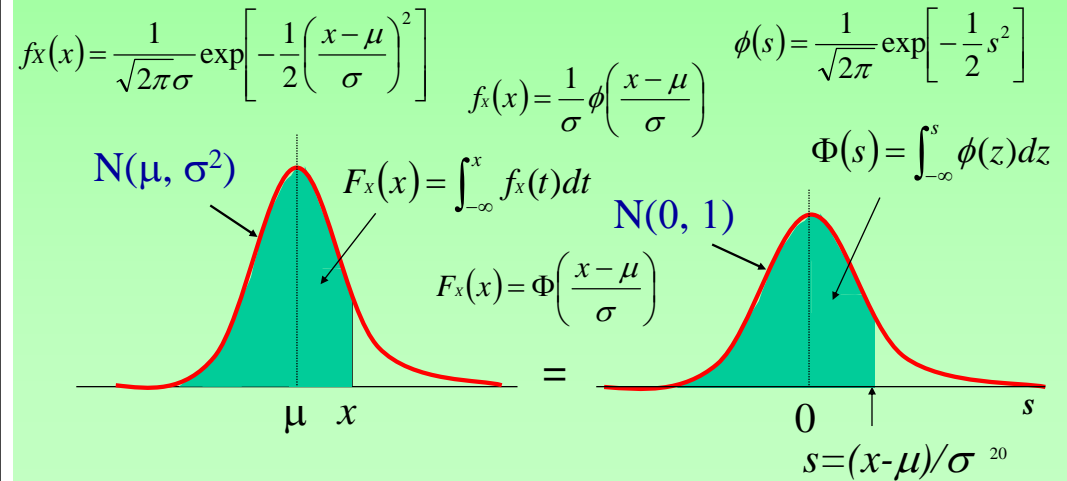
$$= \Phi(-0.675) = 0.25$$

(For $\lambda=5.12, \zeta=0.50$)

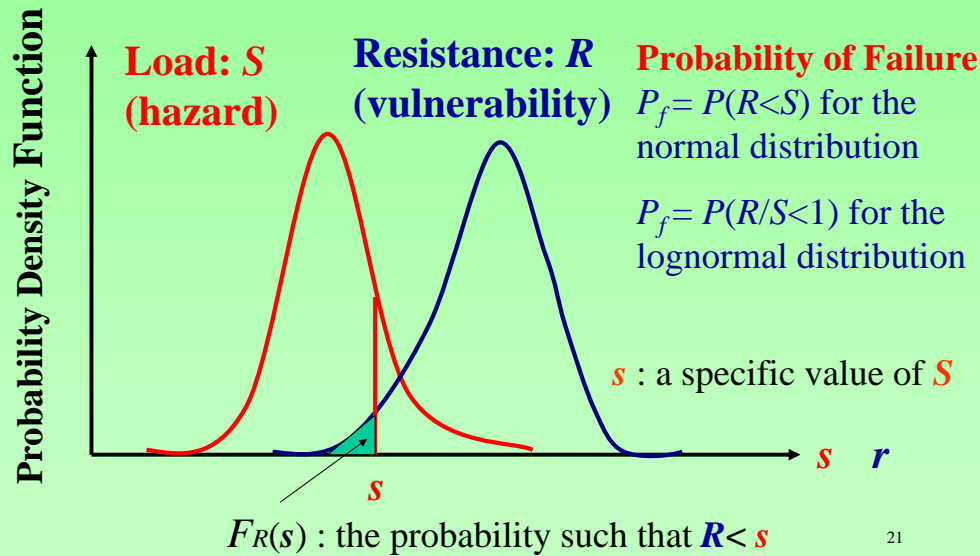
The normal (Gaussian) distribution and the standard normal distribution

PDF (probability density function) of a normal distribution: $N(\mu, \sigma^2)$

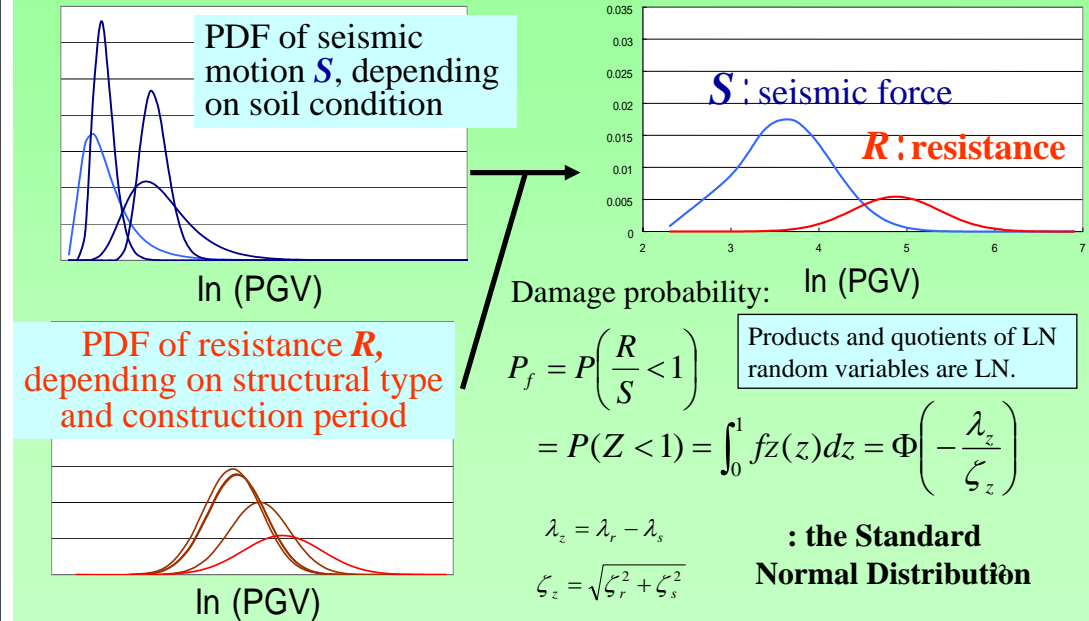
PDF of the standard normal distribution: $N(0, 1)$



Probabilistic Modeling of Load and Resistance and Probability of Failure

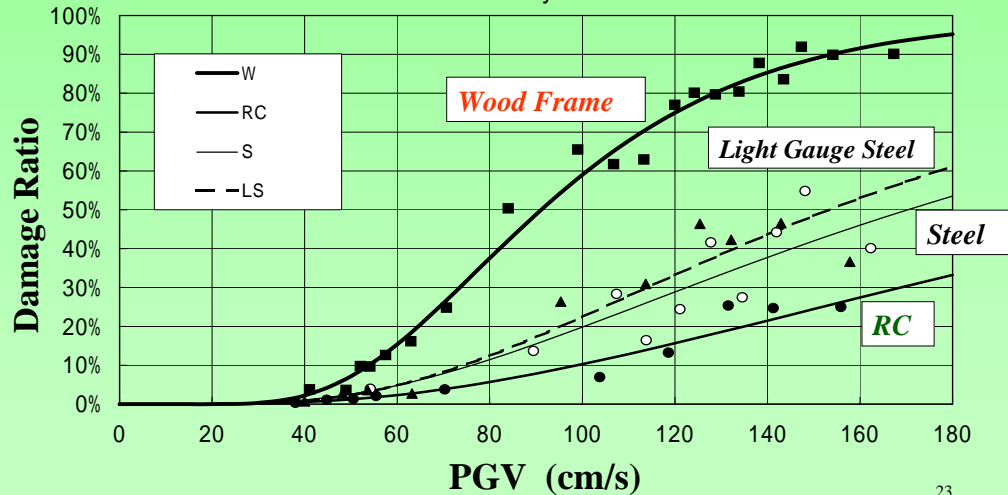


Damage probability of buildings when seismic motion (PGV) is given probabilistically



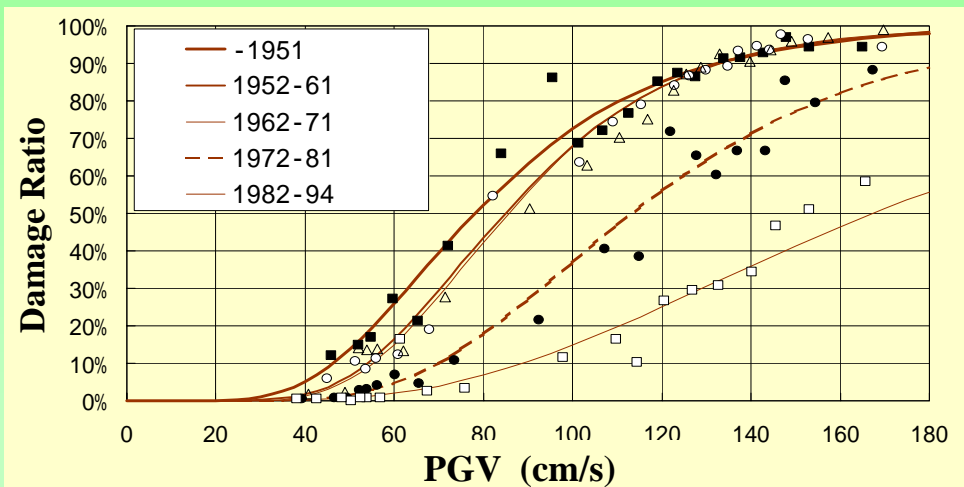
Fragility Curves for different building structures based on the 1995 Kobe EQ

Damage Rank= *Severe Damage (equal or more than severe damage)*

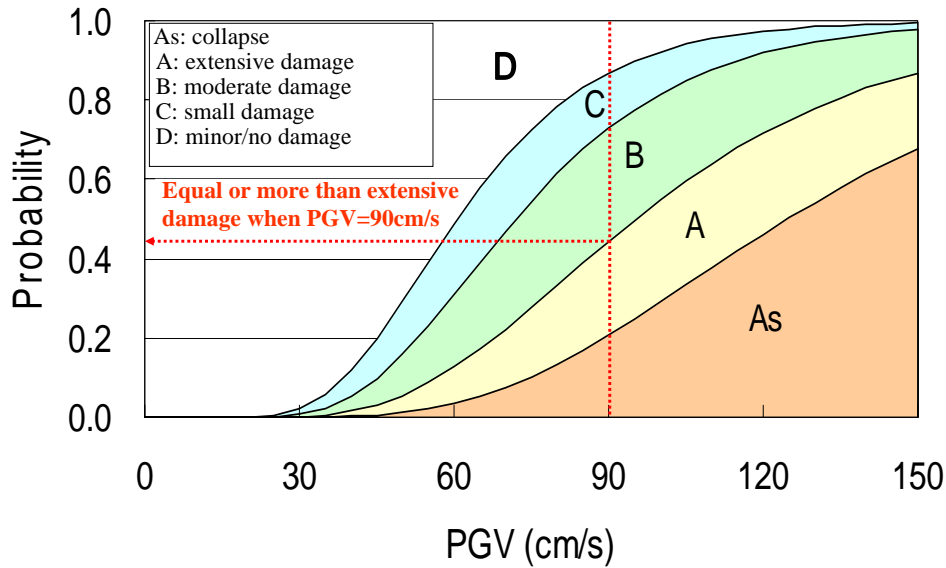


Fragility Curves for Wood-frame Buildings of Different Construction Periods based on the 1995 Kobe EQ

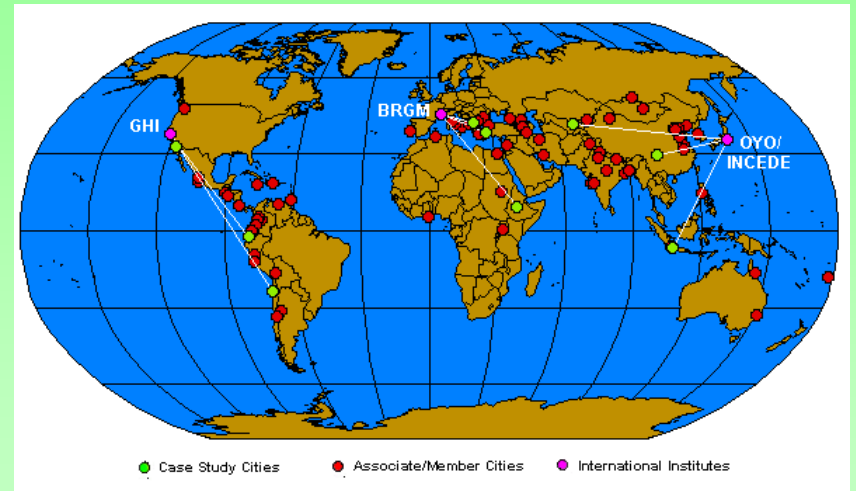
Damage Rank= *Severe Damage (equal or more than severe damage)*



Fragility curves of highway bridges in Japan for various damage levels

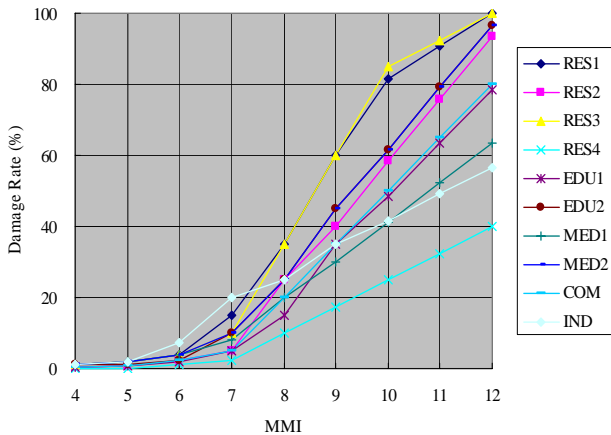


RADIUS (Risk Assessment Tools for Diagnosis of Urban Areas against Seismic Disasters) Project by United Nations



Building fragility curves in a simplified damage assessment tool of RADIUS

Building Damage Curve



MMI (Modified Mercalli Intensity)

ES1--- Informal construction: mainly slums, row housing etc. made from unfired bricks, mud mortar, loosely tied walls and roofs

ES2--- URM-RC composite construction: substandard construction, not complying with the local building code provisions. Height up to 3 stories. URM = Unreinforced Masonry, RC = Reinforced Concrete

ES3--- URM-RC composite construction: old, deteriorated construction, not complying with the latest building code provisions. Height 4 - 6 stories

ES4--- Engineered RC construction: newly constructed multi-story buildings, for residential and commercial purposes

DU1--- School buildings, up to 2 stories: generally, the percentage of this type of building should be very low

DU2--- School buildings, greater than 2 stories: office buildings should also be included in this class; generally, the percentage of this type of buildings should be very low

ED1--- Low to medium rise hospitals: generally, the percentage of this type of building should be very low

Attenuation Model

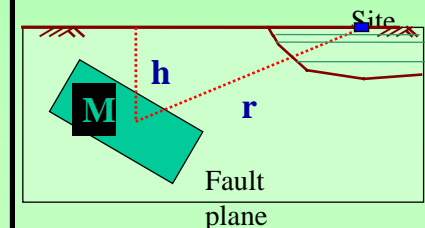
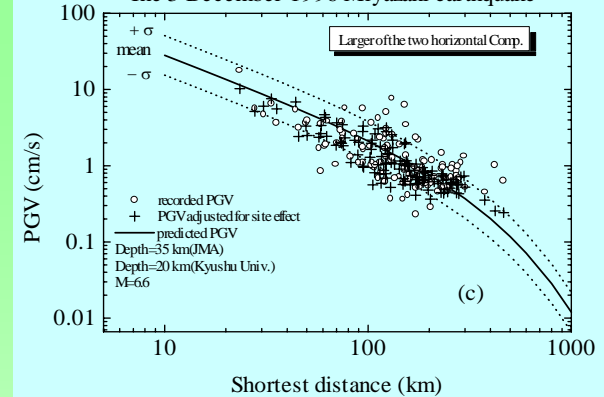
Intensity of Seismic Motion
 $Y = f(\text{Source, Path, Site})$

M, h, r soil classification

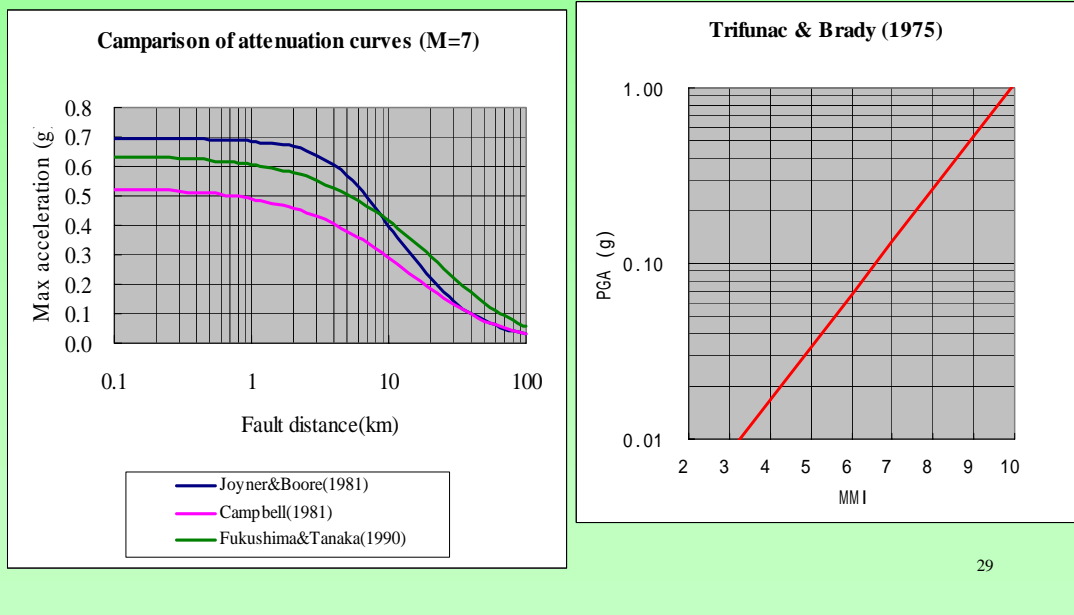
$$Y = b_0 + b_1M + b_2r + b_3\log_{10}r + b_4h + c_i$$

where
Y is \log_{10} PGA, \log_{10} PGV, or JMA seismic intensity,
M is the magnitude
r is the shortest distance to the fault rupture
h is the depth
 b_i are the coefficients to be determined
 c_i is the station coefficient of the recording station i

The 3 December 1996 Miyazaki earthquake

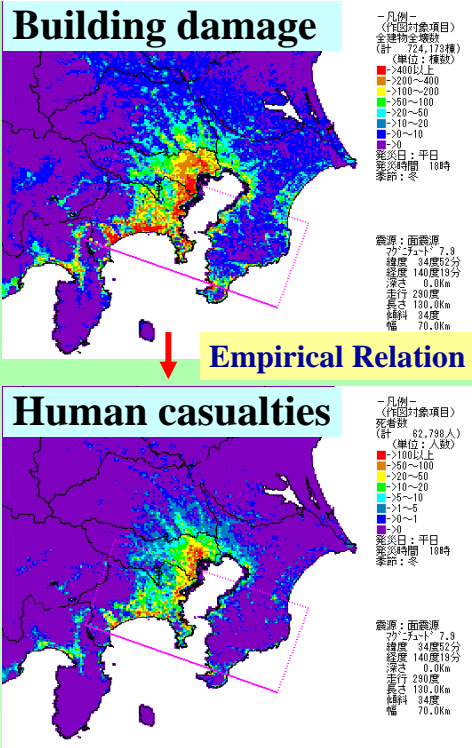
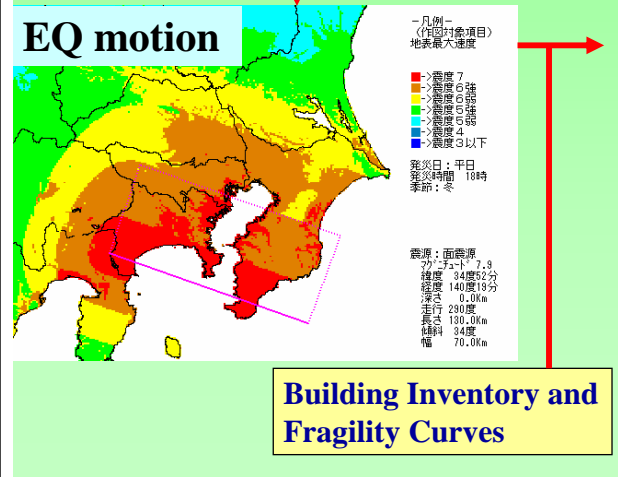


Attenuation relations of PGA and PGA vs MMI relation used in a RADIUS tool



Damage Assessment for Scenario EQ

Scenario EQ: Location, Magnitude, Occurrence time, Season

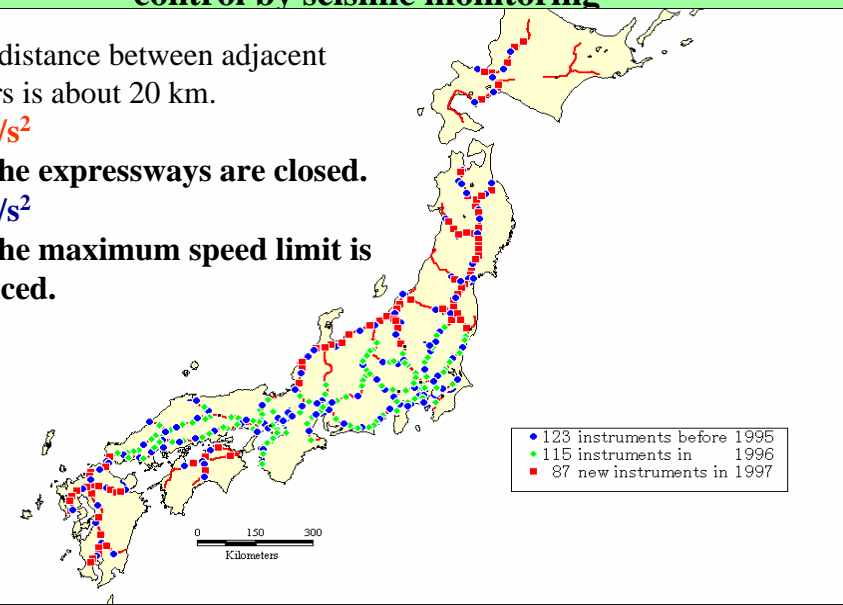


Early Damage Assessment Systems

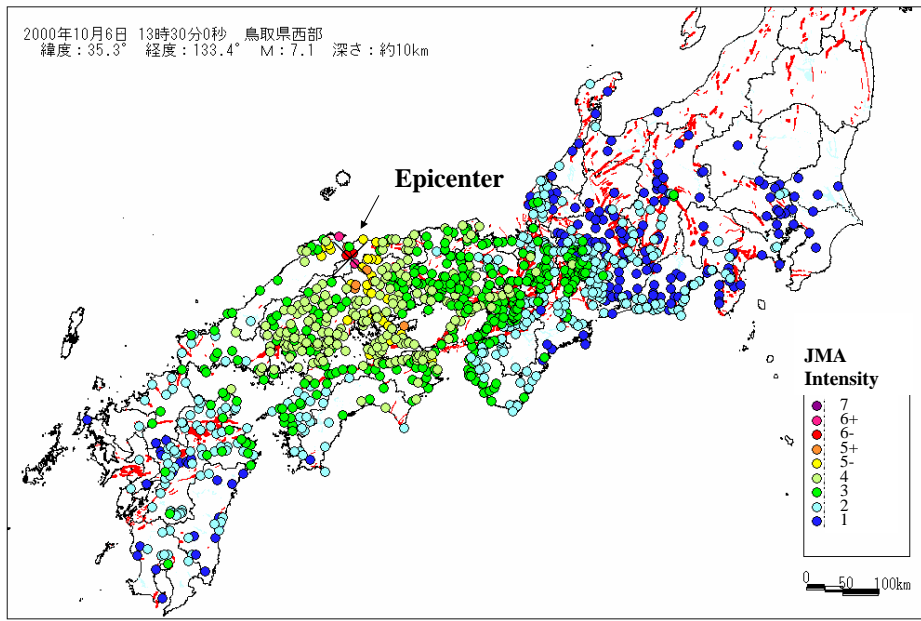
Accelerometers for expressways networks in Japan and traffic control by seismic monitoring

The average distance between adjacent seismometers is about 20 km.

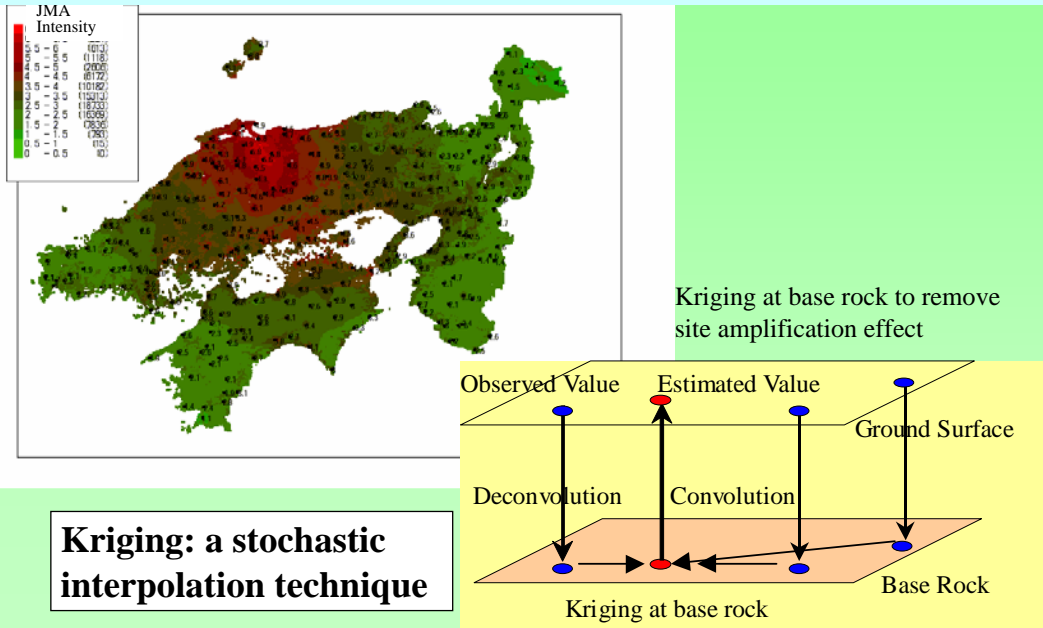
- PGA ≥ 80 cm/s²**
→ The expressways are closed.
- PGA ≥ 50 cm/s²**
→ The maximum speed limit is reduced.



JMA instrumental intensity recorded by national seismic networks in the October 6, 2000 Tottori EQ



Distribution of JMA seismic intensity in the 2000 Tottori EQ estimated by Kriging technique



Kriging: a stochastic interpolation technique

Flow of seismic loss estimation for scenario earthquakes and for real earthquakes

